

Concrete Degradation Modeling Research at NIST

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Similarities to Other Models

- Chemistry of the pore solution
- Dissolution/Precipitation reactions
- Empirical porosity dependence of transport coeff.
- Physics and chemistry treated separately
- Chemical reaction is a boundary condition to transport

Uniqueness at NIST

Modeling concentrated electrolytes

- Activity coefficients: Pitzer
- Solution density: y/γ
- Solution viscosity: $D(c)$
- Equivalent conductivity: $u(c)$

Validation Approach

- Binary/ternary diffusion coefficient
- Solution conductivity
- Transference number
- Diffusion potential

Parameter-free calculations!

Electrolyte

Electro-Diffusive flux:

$$\mathbf{j}_i = -\frac{D_i}{RT} c_i \nabla \mu_i - z_i u_i c_i \nabla \psi \quad \mu_i = \mu_i^\circ + RT \ln y_i c_i$$

Electroneutrality:

$$F \sum_i z_i \mathbf{j}_i = 0$$

Electrical Field:

$$\mathbf{E} = -\nabla \psi = \frac{\frac{F}{RT} \sum_i z_i D_i c_i \nabla \mu_i}{\sum_i z_i^2 F u_i c_i}$$

Implementation Details

$$\dot{\mathbf{j}}_i = -\frac{D_i}{RT} c_i \nabla \mu_i - z_i u_i c_i \nabla \psi$$

Diffusion Coefficient:

$$D_i = D_i^s \left(\frac{\eta_w}{\eta_{soln}} \right)^{1.0}$$

Viscosity:

$$\left(\frac{\eta_{soln}}{\eta_w} \right) = 1 + \sum_i A_i c_i^{1/2} + B_i c_i$$

Implementation Details

$$\mathbf{j}_i = -\frac{D_i}{RT} c_i \nabla \mu_i - z_i u_i c_i \nabla \psi$$

Electrochemical Mobility:

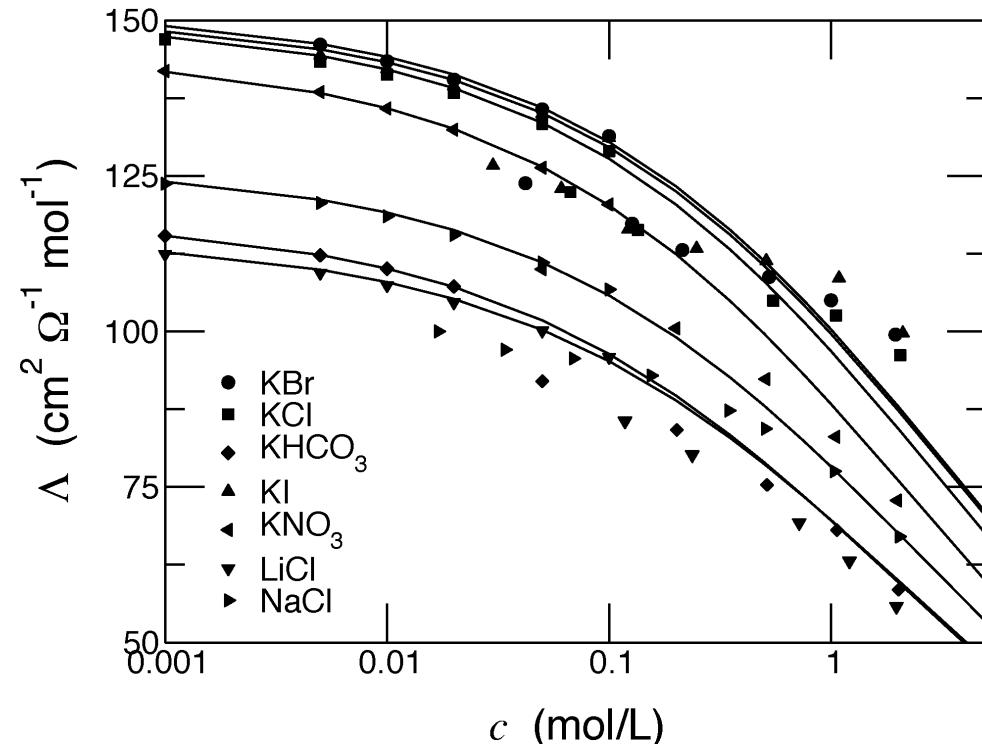
$$\Lambda = \sum_i \lambda_i$$

$$\lambda_i = F u_i$$

$$\lambda_i = \frac{\lambda_i^o}{1 + G_i I_c^{1/2}}$$

Conductivity:

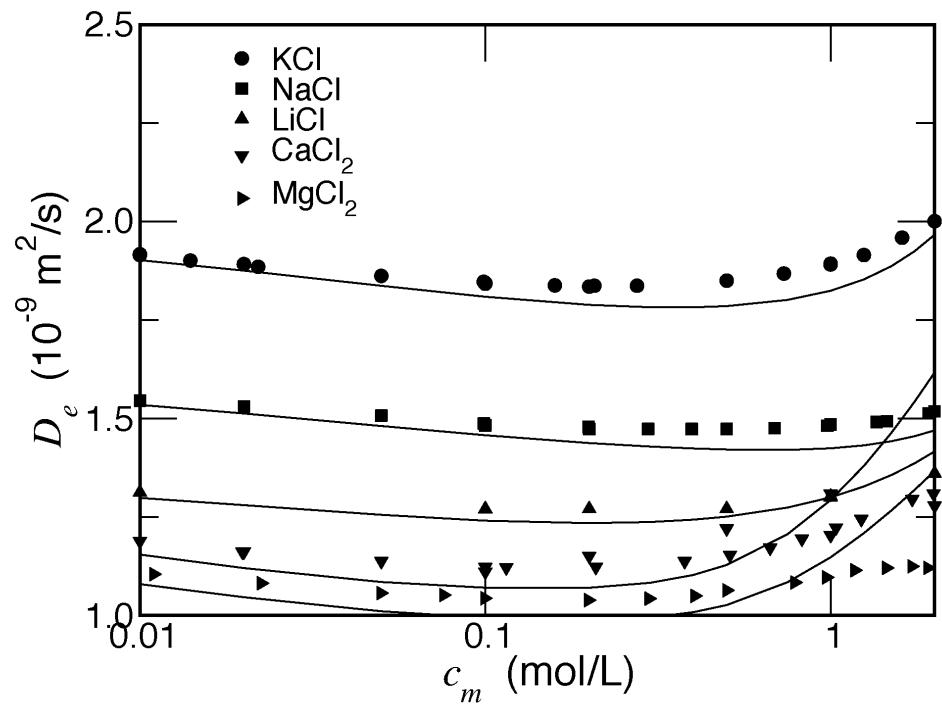
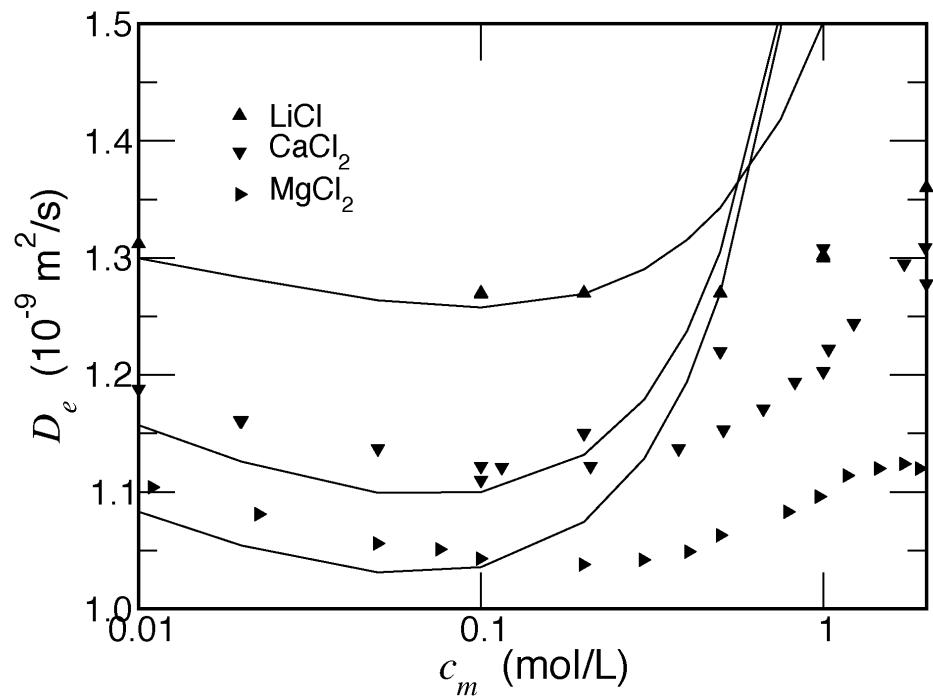
$$\sigma = \sum_i z_i^2 c_i \lambda_i$$



Binary Diffusion

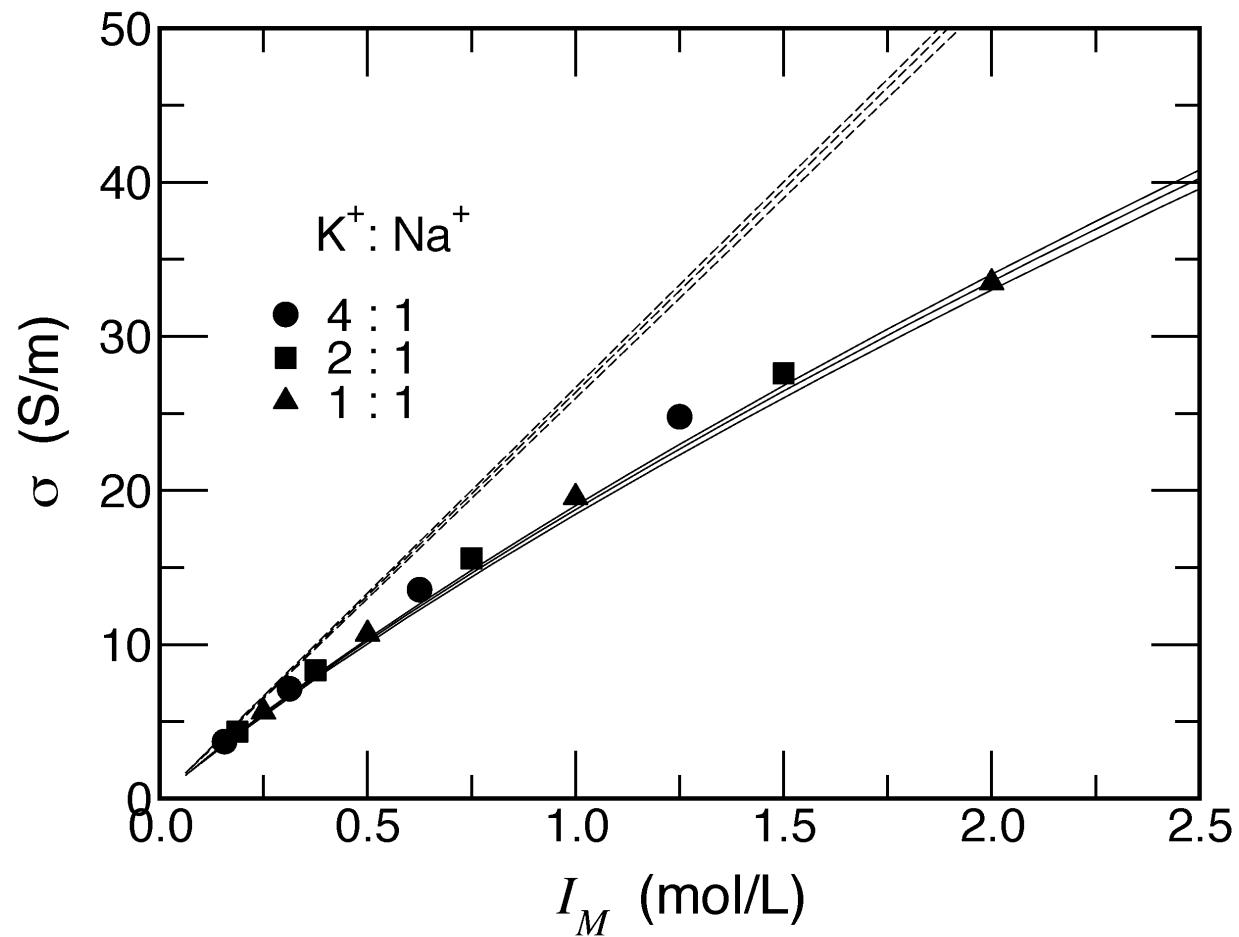
$$D_i = D_i^s$$

$$D_i = D_i^s \left(\frac{\eta_w}{\eta_{soln}} \right)$$



Solution Conductivity

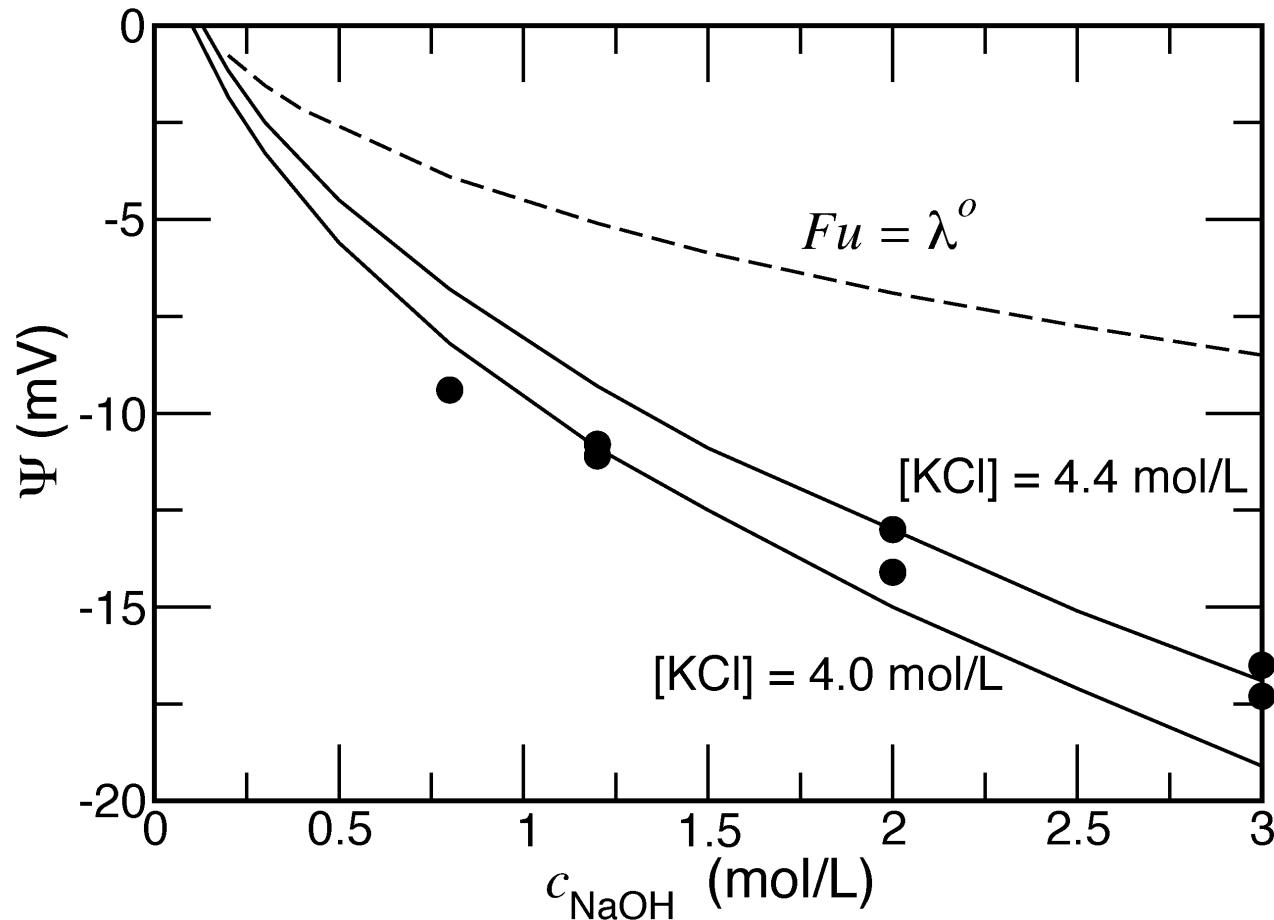
KOH + NaOH



Snyder, Feng, Keen, and Mason, *Cem. Concr. Res.*, 33, 793-798, 2002.

Liquid Junction Potential

$\text{KCl}(\text{sat}) \parallel \text{NaOH}$

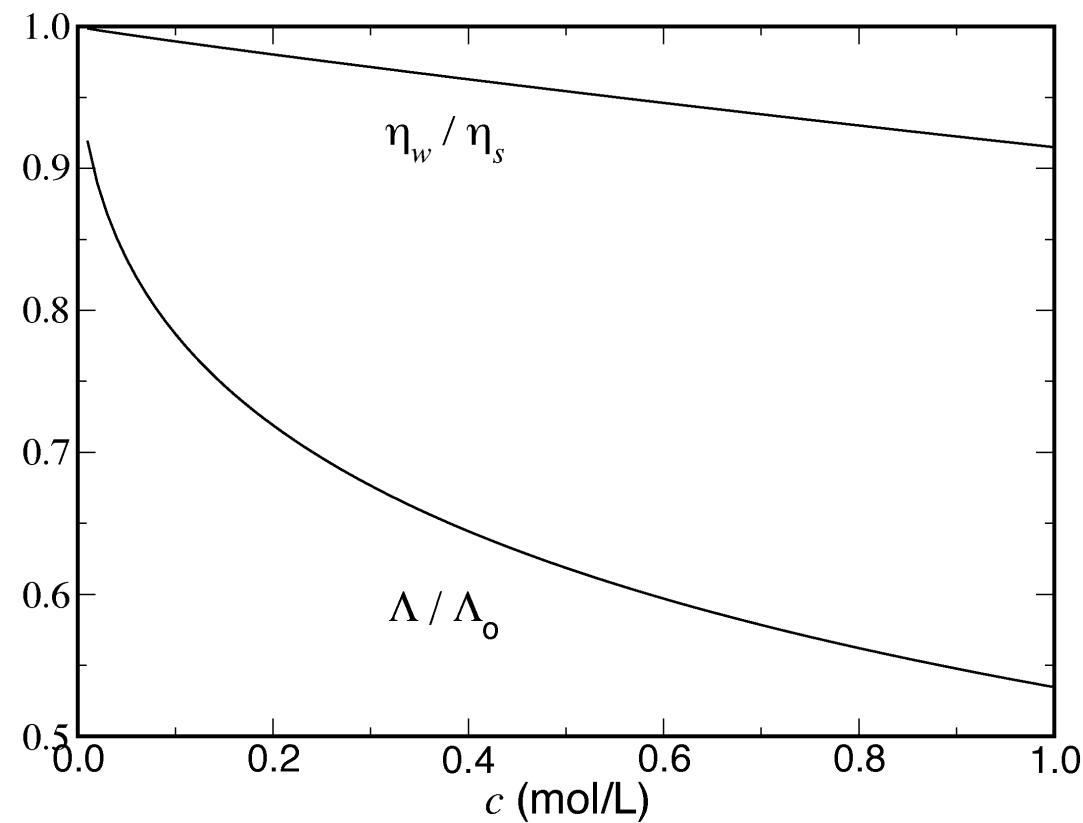


Norkus and Vaskelis, *Electroanalysis*, 8, 171-172, 1996.

D(c) vs. u(c)

$$\frac{\eta_w}{\eta_{\text{soln}}} \quad \text{vs.} \quad \sum_i \frac{1}{1 + G_i I_M^{1/2}}$$

NaCl



Bulk Transport

Pore Space:

$$\mathbf{j}_i^p = \tau^{-1} \mathbf{j}_i$$

Bulk Porous Material:

$$\mathbf{j}_i^b = \frac{\theta}{\tau} \mathbf{j}_i$$

Bulk Transport:

$$\mathbf{j}_i^b = -\frac{LD_i}{RT} c_i \nabla \mu_i - z_i L u_i c_i \nabla \psi \quad L = \frac{\theta}{\tau}$$

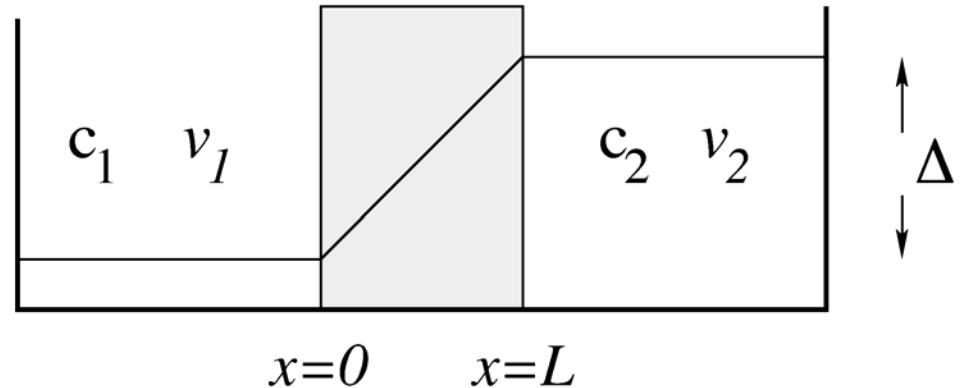
Laboratory Validation

- Alumina frit: 500 nm pores
- Temperature control: 25 °C
- Potassium Iodide: I⁻
- Counter-diffusing binary salt
- Constant water activity
- Formation Factor: $L = \sigma_{\text{bulk}} / \sigma_{\text{soln}}$

Laboratory Validation

Assumption: Fick's Law

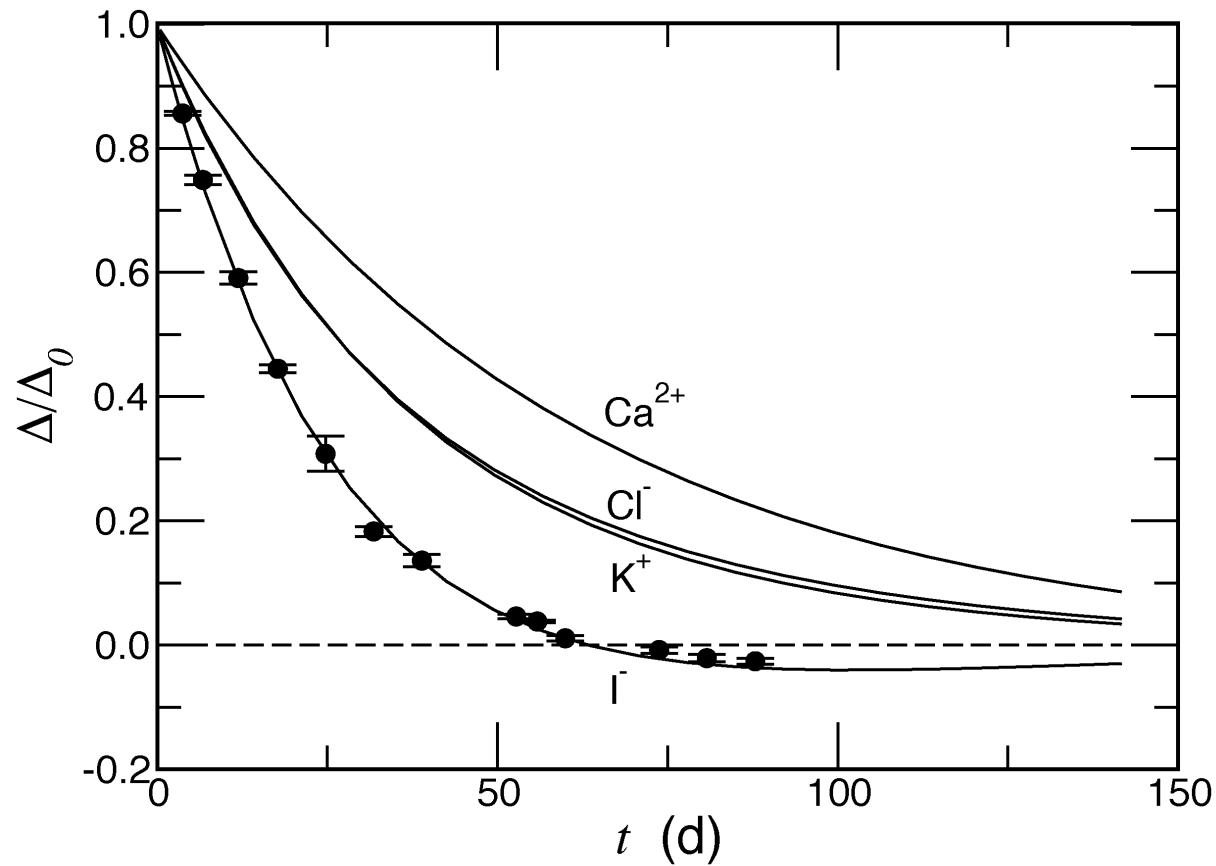
- Flux is constant
- $\Delta_o = (c_2 - c_1)$ at $t = 0$
- $\Delta = c_2 - c_1$



$$\frac{\Delta}{\Delta_o} = \exp \left[\frac{-AD^*}{L} \left(\frac{1}{v_1} + \frac{1}{v_2} \right) t \right]$$

Laboratory Validation

KI - CaCl₂



Snyder and Marchand, *Cem. Concr. Res.*, **31**, 1837-1845, 2001.

Bulk Migration: Applied Voltage

Macroscopic Electroneutrality: $l \gg \kappa^{-1}$

$$\frac{\partial \rho}{\partial t} = \nabla \cdot \mathbf{J} = 0$$

$$\nabla \cdot \mathbf{J} = 0$$

$$\Delta V_n = \tilde{V} \frac{1/\sigma_n}{\sum_n 1/\sigma_n} \quad \tilde{V} = V_{ext} - V_{DP}$$

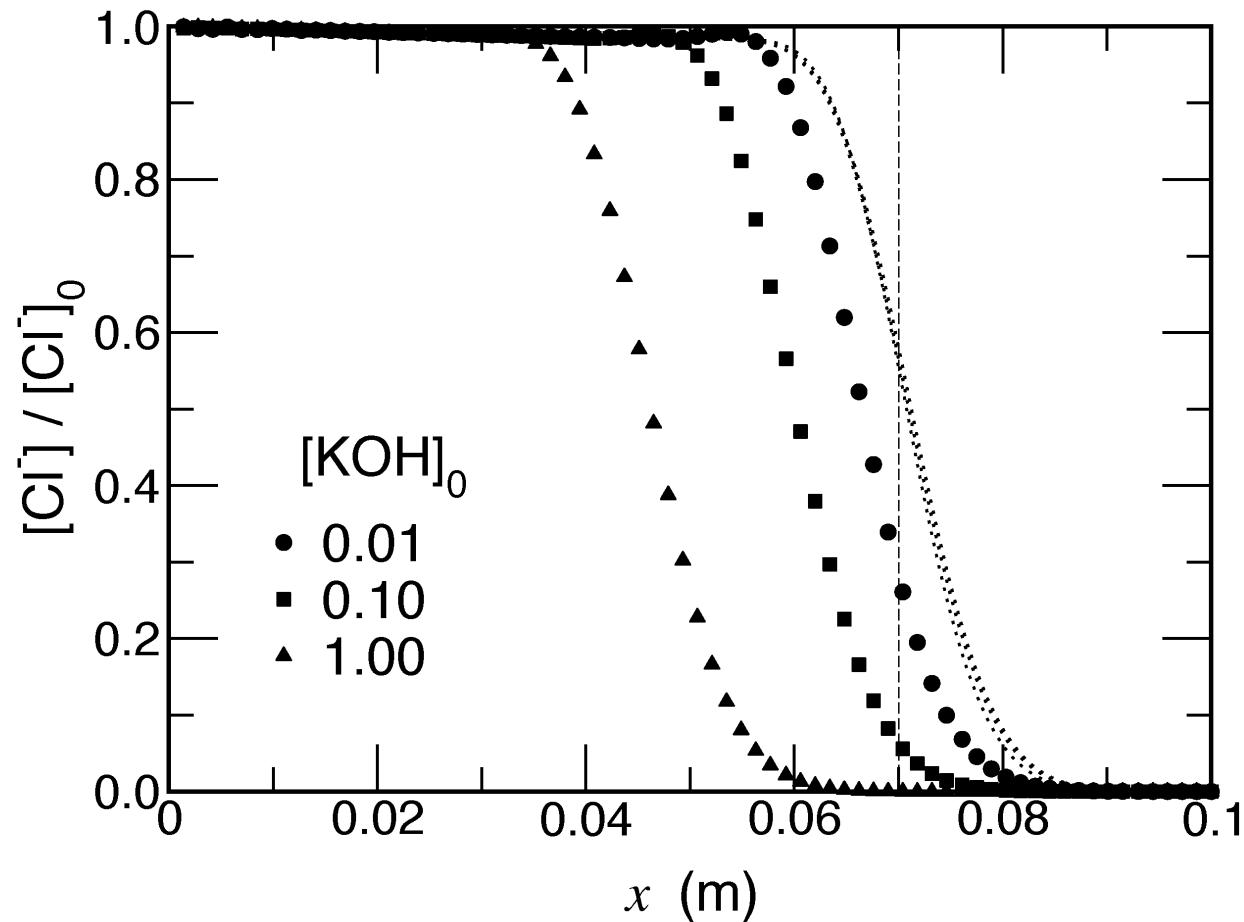
Bulk Migration: Applied Voltage

$$L = 0.10 \text{ m}$$

$$A = 0.001 \text{ m}^2$$

$$\psi_{\text{ext}} = 10 \text{ V}$$

$$\frac{[\text{NaCl}]}{[\text{KOH}]} = 0.01$$



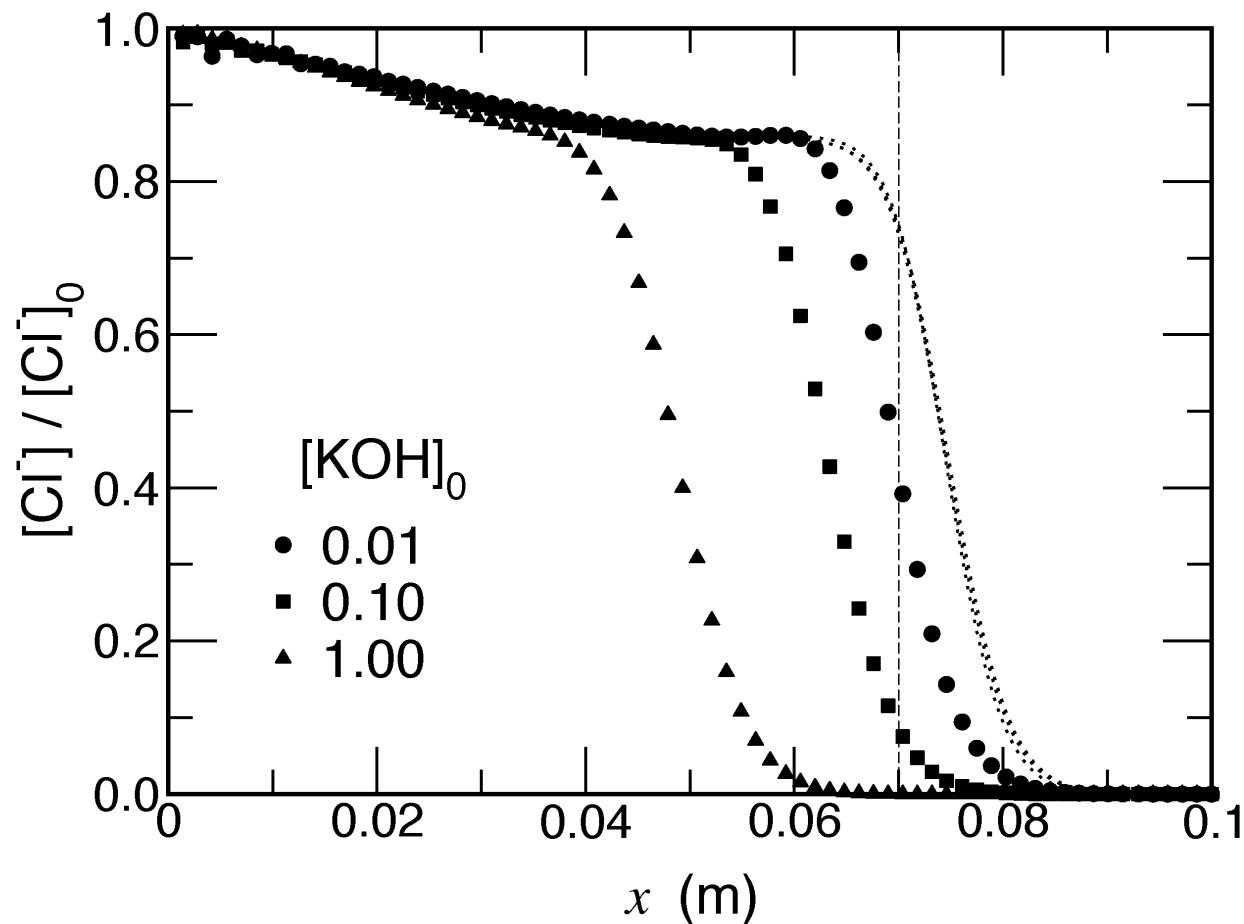
Bulk Migration: Applied Voltage

$$L = 0.10 \text{ m}$$

$$A = 0.001 \text{ m}^2$$

$$\psi_{\text{ext}} = 10 \text{ V}$$

$$\frac{[\text{NaCl}]}{[\text{KOH}]} = 0.10$$



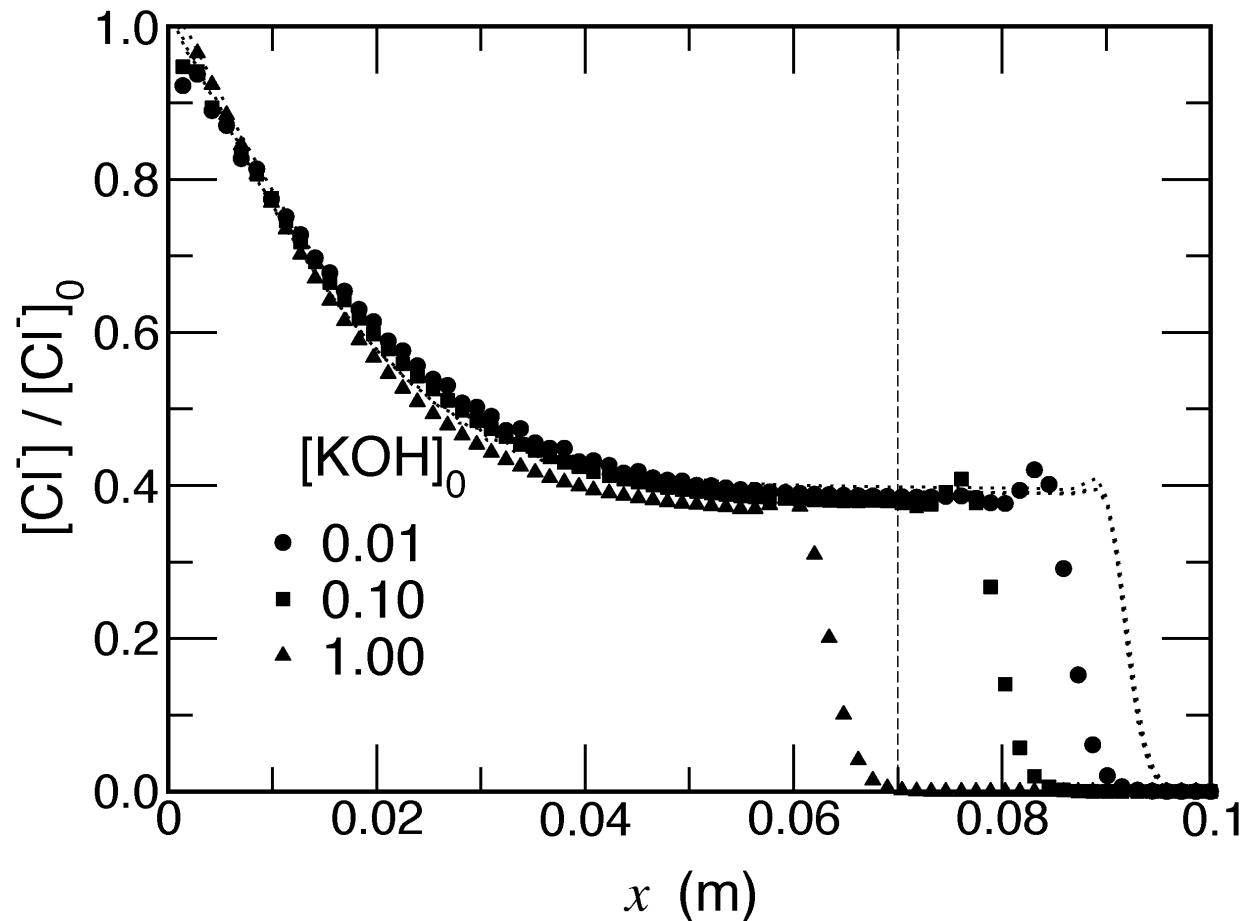
Bulk Migration: Applied Voltage

$$L = 0.10 \text{ m}$$

$$A = 0.001 \text{ m}^2$$

$$\psi_{\text{ext}} = 10 \text{ V}$$

$$\frac{[\text{NaCl}]}{[\text{KOH}]} = 1.00$$



Future Work

- Redox reactions and kinetics
- Osmotic effects
- Moisture transport
- Temperature dependence
- Binding